

Technical photosynthesis involving CO₂ electrolysis and fermentation

Thomas Haas¹, Ralf Krause², Rainer Weber³, Martin Demler¹ and Guenter Schmid^{2*}

Solar-powered electrochemical reduction of CO₂ and H₂O to syngas, followed by fermentation, could lead to sustainable production of useful chemicals. However, due to insufficient electric current densities and instabilities of current CO₂-to-CO electrolyzers, a practical, scalable artificial photosynthesis remains a major challenge. Here, we address these problems using a commercially available silver-based gas diffusion electrode (used in industrial-scale chlorine-alkaline electrolysis) as the cathode in the CO₂ electrolyser. Electric current densities up to 300 mA cm⁻² were demonstrated for more than 1,200 hours with continuous operation. This CO₂ electrolyser was coupled to a fermentation module, where the out-coming syngas from the CO₂ electrolyser was converted to butanol and hexanol with high carbon selectivity. Conversion of photovoltaic electricity, CO₂ and H₂O to the desired alcohols achieved close to 100% Faradaic efficiency. Industrial production of useful and high-value chemicals via artificial photosynthesis is closer than expected with the proposed scalable hybrid system.

High-value organic chemicals, such as butanol and hexanol, have multiple applications in coatings, chemical synthesis, and as solvents and fuels. Currently, about four million metric tonnes of 1-butanol are produced worldwide. In Germany, about 0.6 million metric tonnes of 1-butanol are produced from fossil fuels per year¹. Until now, these organic chemicals have been produced largely from oil. This production is complex, costly and is not sustainable due to limited oil sources. The value that is addressed here is the ratio between the commercial price of butanol (1.2€ per kg) and its heat of combustion (10.80 kWh per kg) = 0.11€ per kWh relative to that of methane (≈0.15€ per kg):(15.42 kWh per kg) = 0.01€ per kWh.

At the end of their life cycle, most organic chemicals end up in the atmosphere as the greenhouse gas CO₂, the concentration of which is rapidly and continuously rising. Attempts are therefore being made to generate organic chemicals from CO₂ and water powered by renewable electricity as so-called 'artificial photosynthesis'²⁻⁴. However, relative to fossil fuels, renewable energy has a low energy density (for example, in Germany, installed renewable electric power generating 100 GW from a combination of photovoltaics (PV), windmills and biomass combustion is distributed over almost 400,000 square kilometres; https://www.energy-charts.de/power_inst_de.html). Therefore, it is necessary to decentralize industrial production of organic chemicals from CO₂ and water via electro-catalysis, to be smaller scale and to run with less chemical infrastructure⁵⁻⁷. By-product accumulation is typical, for example in the Fischer-Tropsch process⁸, and thus elaborate separation techniques must also be avoided. This favours the involvement of microorganisms as they are often more selective than chemical catalysts to produce desired organic compounds. The Faradaic efficiency (efficiency of electron transfer into products) must be high in terms of converting all electricity into only the desired products. This favours the involvement of anaerobic microorganisms. If aerobic microorganisms are involved, a significant portion of the electrons can end up in water, increasing the electricity demand. Further, anaerobic fermenters are less expensive (there is less corrosion and in many cases sterilization is not required) than aerobic ones.

Herein, we describe the production of butanol and hexanol from CO₂, H₂O and renewable energy and how such a decentralized industrial plant with a capacity of a few 10,000 tonnes of butanol and/or hexanol per year might operate. A conventional PV module providing electricity with an energy conversion efficiency of around 20% (ref. ⁹), a CO₂ electrolyser constantly operating at high current densities and a bioprocess module for the anaerobic conversion of CO, H₂ and CO₂ (syngas) to the desired alcohols were employed (Fig. 1 and Supplementary Fig. 1).

Results

Initial considerations. The CO₂ electrolyser in the hybrid system is the heart of this technical photosynthesis (Fig. 1) as it produces a mixture of mainly CO and H₂ (syngas of various composition) from electricity and CO₂ and H₂O. The lower redox potential of the CO/CO₂ couple ($E_0' = -520$ mV) as compared to that of the H⁺/H₂ couple ($E_0' = -414$ mV) allows for anaerobic bacteria to perform a number of reduction reactions, such as reduction of carboxylic acids to their respective aldehydes ($E_0' = -580$ mV), or the reductive carboxylation of acetyl-CoA to pyruvate ($E_0' = -500$ mV). These reactions are thermodynamically and kinetically unfavourable; if H₂ was the sole electron donor in conjunction with CO₂ as the carbon source¹⁰, practically no alcohols or pyruvate-derived products would be formed^{11,12}. Therefore, the presence of CO is essential to gain the desired product selectivity.

For an industrial-scale electrochemical reduction, CO₂ concentrations higher than atmospheric concentrations are needed to produce larger concentrations of CO. Renewable sources of CO₂ include breweries, anaerobic digestion plants and power plants that convert biomass into electricity. CO₂ is also a side product of cement and steel production¹³. All of these CO₂ production sites are widely dispersed. CO₂ can also be concentrated from the atmosphere (0.04%) at a theoretical energy cost of at least 20 kJ mol⁻¹. Carbon capture from the atmosphere cannot be centralized because scrubbing out 1 mol CO₂ (44 g) requires at least 56,000 litres of air, which is another reason why industrial production of organic chemicals from CO₂ and H₂O should be decentralized.

¹Evonik Creavis GmbH, Marl, Germany. ²Siemens AG, Erlangen, Germany. ³Covestro AG, Leverkusen, Germany. Ralf Krause and Martin Demler contributed equally to this work. *e-mail: guenter.schmid@siemens.com

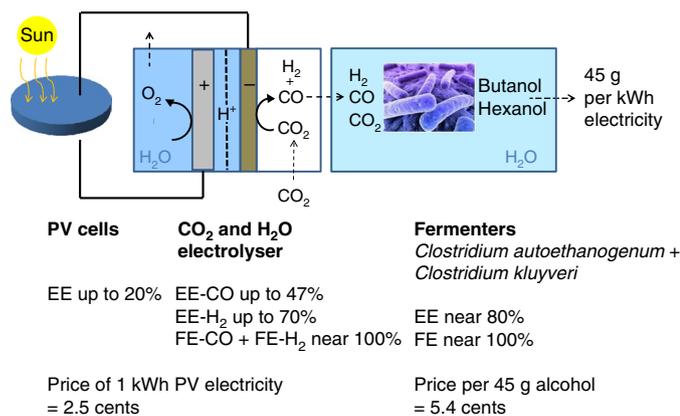


Fig. 1 | Sketch of the modules used in technical photosynthesis of

1-butanol and 1-hexanol from CO₂ and H₂O. For a detailed structure of the CO₂ electrolyser see Fig. 2a and for process design of the fermenters see Supplementary Fig. 1. PV, photovoltaic; EE, energy conversion efficiency; FE, Faradaic efficiency. Cents are 0.01€. At a PV-cell energy conversion efficiency of 20%, the overall energy conversion efficiency is above 8%. For calculation of the amount of butanol and hexanol obtained per kWh and for cost calculations see Methods. At present prices, the value of the alcohols formed is 2.2 fold higher than the price of the PV electricity consumed. Butanol costs 1.2€ per kg (ref. 1). In the fermenters, syngas produced by the CO₂ electrolyser was converted first to acetate and ethanol by the anaerobic bacterium *Clostridium autoethanogenum*. Secondly, acetate and ethanol were fermented to butyrate and hexanoate by *C. kluyveri*; and thirdly, butyrate and hexanoate were reduced by CO and H₂ to butanol and hexanol, respectively, by *C. autoethanogenum*⁵⁰.

CO₂ electrolyser. In CO₂ electrolysers, CO₂ rather than HCO₃⁻ or CO₃²⁻ is reduced at a gas diffusion cathode¹⁴. Furthermore, CO₂ has a low solubility in salt-based electrolytes. Thus, the electric current density at the cathode's surface is generally too low for carrying out any technical applications (only a few mA cm⁻²) when operating the electrolyser at a CO₂ pressure of 1 bar and ambient temperature^{15–21}, despite the fact that the Faradaic and energy conversion efficiencies are high^{22,23}. We solved this problem by letting the gas diffusion cathode interact at its opposite side with 100% gaseous CO₂ rather than dissolved CO₂ (Fig. 2a). Covestro recently introduced such an operation mode in industrial chlorine-alkaline electrolysis called oxygen depolarization cathode (ODC) (cathode reaction: $\frac{1}{2}\text{O}_2 + \text{H}_2\text{O} + 2\text{e}^- \rightarrow 2\text{OH}^-$; anode reaction: $2\text{Cl}^- - 2\text{e}^- \rightarrow \text{Cl}_2$; <https://www.covestro.com/en/sustainability/lighthouse-projects/sauerstoffverzehrkathode>), which can work at electric current densities of more than 400 mA cm⁻² (ref. 24). There ODC was introduced to suppress the hydrogen evolution reaction (HER) and therefore decrease cell voltage and increase energy efficiency. Surprisingly, these commercially available gas diffusion electrodes also work in CO₂ electrolysis.

At this silver-based cathode, CO₂ was reduced to CO ($\text{CO}_2 + \text{H}_2\text{O} + 2\text{e}^- \rightarrow \text{CO} + 2\text{OH}^-$) and at the iridium-oxide-coated titanium anode^{25,26}, water was oxidized to O₂ ($\text{H}_2\text{O} - 2\text{e}^- \rightarrow \frac{1}{2}\text{O}_2 + 2\text{H}^+$). In close proximity of the cathode, the pH becomes very basic ($\text{CO}_2 + \text{H}_2\text{O} + 2\text{e}^- \rightarrow \text{CO} + 2\text{OH}^-$), which in the bulk catholyte is neutralized by excess of CO₂ ($2\text{OH}^- + 2\text{CO}_2 \rightarrow 2\text{HCO}_3^-$). Thus, the overall cathode chamber reaction is: $3\text{CO}_2 + \text{H}_2\text{O} + 2\text{e}^- \rightarrow \text{CO} + 2\text{HCO}_3^-$. In other words, three CO₂ molecules have to be supplied to the gas diffusion electrode to accomplish electrochemical reduction of one CO₂.

The current-voltage characteristic of the CO₂ electrolyser (Fig. 2a) is depicted in Fig. 2b. The electric current density increased with increasing voltage and temperature. Extrapolation to zero current density yielded a minimal cell voltage of 2.3 V. The increase in

current density was due to an increase in electrolyte conductivity when the temperature was raised from 30 °C to 60 °C.

At the silver-based gas diffusion electrode of the gas-to-gas CO₂ electrolyser (Fig. 2a), not all the CO₂ supplied could be converted to CO, and H₂ was competitively formed by proton reduction (HER). CO-Faradaic efficiency and H₂-Faradaic efficiency still totalled around 100%, because no other gaseous products were formed. The formation of traces of formic acid²⁷ can be neglected. The CO to H₂ ratio depends on the CO₂-supply rate (Fig. 2c and Table 1), because the rate of CO₂ reduction to CO at a given current density is kinetically limited by the diffusion of CO₂ to and CO from the cathode in the presence of a huge excess of H₂O. In contrast to most literature, our electrolysers were continuously operated far away from the thermodynamic limit to yield an industrially applicable current density. The maximum volumetric CO formation rate $\dot{V}_{\text{CO}_{\text{max}}}$ (l s⁻¹) is given by the total cell current I_{cell} (A)

$$\dot{V}_{\text{CO}_{\text{max}}} = \frac{V_{\text{CO}_{\text{mol}}}}{z \times F} \times I_{\text{cell}}$$

$\dot{V}_{\text{CO}_{\text{max}}}$ is the molar volume of CO (22.41 mol⁻¹), F is the Faraday constant (96,485 A s mol⁻¹), and z is the number of electrons required to reduce CO₂ to CO, which is two. In order to characterize the operation conditions, we introduced the experimental parameter λ as the ratio of the volumetric CO₂ supply rate \dot{V}_{CO_2} (l s⁻¹) and $\dot{V}_{\text{CO}_{\text{max}}}$

$$\lambda = \frac{\dot{V}_{\text{CO}_2}}{\dot{V}_{\text{CO}_{\text{max}}}}$$

Usually, $\lambda > 3$ is required to sufficiently reduce the competing HER. λ increases with increasing CO₂ flow rate and decreases with increasing electric current density. Furthermore, catholyte and anolyte are continuously mixed to ensure constant pH, K⁺ and HCO₃⁻ concentration during the course of the long-term experiment.

At 300 mA cm⁻² and a CO₂ flow rate of 90 sccm ($\lambda = 4.78$) the Faradaic efficiency for CO was near 70% and that for H₂ near 30% (Fig. 3a), and both remained almost constant within experimental error for more than 1,200 h (Fig. 3b) due to anolyte and catholyte mixing. Such high CO-Faradaic efficiencies at high current densities have in the past only been achieved for minutes under specific conditions, where in the electrolyser the electrolyte was cycled only once through the electrolysis cell and then discarded¹⁸ or when electrocatalytic CO₂ reduction to CO was performed at high CO₂ pressure (>15 atm)²¹.

The minimum cell voltage of 2.3 V (Fig. 2b) corresponds to a theoretical maximum total (CO+H₂) energy efficiency of 64%, assuming an adiabatic cell potential of 1.47 V (for calculation see Methods). With increasing current density the CO energy conversion efficiency decreased (Fig. 3a). At 300 mA cm⁻², the total energy efficiency for CO and H₂ dropped to nearly 20%. Therefore, when CO:H₂ ratios lower than around 2:1 (Fig. 3b) are anticipated, it is more energy efficient to use in parallel a separate H₂O electrolyser rather than to increase the electric current density in the CO₂ electrolyser. H₂O-electrolysers operate stably at electric current densities of, for instance, 1.5 A cm⁻² at around 2 V with an energy efficiency of around 70% (ref. 28).

The syngas collected was almost free of O₂ (<<100 ppm), because the catholyte was separated from the site of CO₂ reduction by the gas diffusion electrode. Any O₂ diffusing into the cathode from the front side or dissolved in the electrolyte was reduced to OH⁻ (ODC reaction), which reacted with CO₂ to form HCO₃⁻ (Fig. 2a). The concentration of this O₂ was very low, as can be deduced from the Faradaic efficiency of CO₂ and H₂O reduction to CO and H₂, respectively, which was found to be nearly 100%. Very low O₂ concentrations in the out-coming

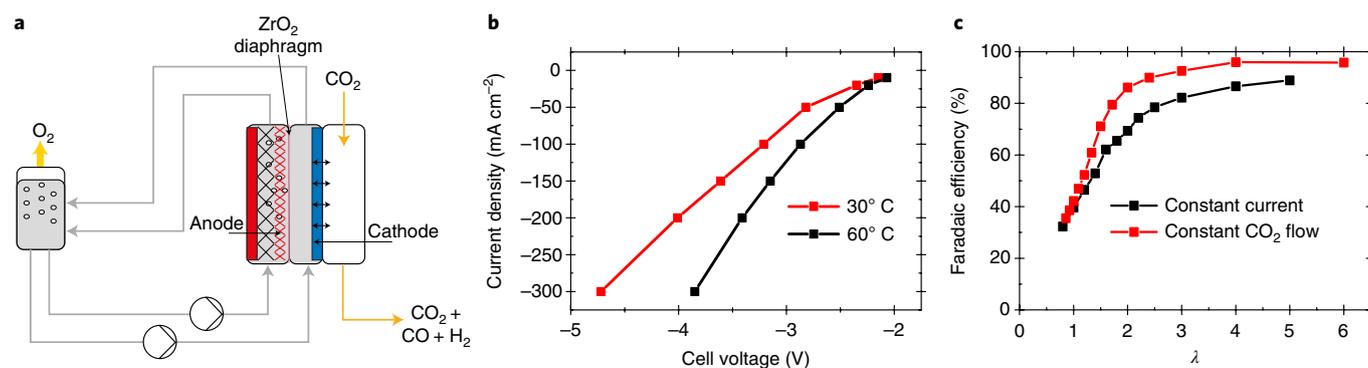


Fig. 2 | Scheme and properties of the CO₂ electrolyser. **a**, The cathode was a silver-based gas diffusion electrode and the anode an iridium-oxide-coated titanium anode with a zero-gap structure. CO₂ was allowed to flow only at the electrolyte opposite the cathode with an effective surface area of 10 cm². The anolyte and the catholyte solutions, both 0.1M K₂SO₄/1.5M KHCO₃ (pH ≈ 7), were continuously cycled and mixed at a flow rate of 200 ml min⁻¹. The temperature was 30 °C. The cathode and the anode were 2 mm apart and separated by a high-conductivity, zirconium-oxide-based diaphragm. **b**, Dependence of the electric current density on the voltage and temperature. The CO₂ flow rate was 10.5 sccm (standard cubic centimetre per min). **c**, Faradaic efficiency of CO summarized from the data given in Table 1.

syngas are of importance, as higher concentrations are toxic for the bacteria converting the syngas to butanol and hexanol in the fermentation phase.

Table 1 | Dependence of the CO Faradaic efficiency (FE-CO) on the experimental variables

CO ₂ flow (sccm)	λ	FE-CO (%)	U _{cell} (V)
Constant current density J = 150 mA cm⁻²			
52.5	5	88.9	4.91
42	4	86.6	4.91
31.5	3	82.2	4.92
26.25	2.5	78.5	4.93
23.1	2.2	74.4	4.93
21	2	69.4	4.93
18.9	1.8	65.5	4.94
16.8	1.6	62.1	4.94
14.7	1.4	52.9	4.95
12.6	1.2	46.5	4.95
10.5	1	39.7	4.96
8.4	0.8	32.3	4.96
J (mA cm ⁻²)	λ	FE-CO (%)	U _{cell} (V)
Constant CO₂ flow at 10.5 ml min⁻¹			
25	6	95.8	2.66
37.5	4	96.0	3.11
50	3	92.6	3.45
62.5	2.4	90.0	3.75
75	2	86.1	4.01
87.5	1.71	79.5	4.23
100	1.5	71.1	4.38
112.5	1.33	60.9	4.52
125	1.2	52.3	4.67
137.5	1.09	46.9	4.81
150	1	42.2	4.97
175	0.86	35.5	5.30

The dependence of the CO Faradaic efficiency (FE-CO) on the CO₂ supply rate, on the electrical current density and on λ (for definition see text). The cathode and the anode were 9.5 mm apart and separated by a high-conductivity, zirconium-oxide-based diaphragm.

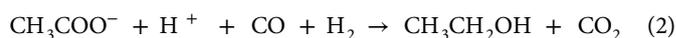
During development of the CO₂ electrolyser described above we first experimented with a preliminary operational mode shown and described in Supplementary Fig. 2a. The main differences were independent electrolyte cycling and H₂SO₄ as anolyte. At current densities of 50 mA cm⁻², this CO₂ electrolyser also generated CO at high Faradaic efficiency for more than 1,000 h (Supplementary Fig. 3), but the CO Faradaic efficiency decreased more with increasing current density than in the setup shown in Fig. 2a. We coupled this preliminary CO₂ electrolyser with a commercially available PV module and measured the power dependence on the voltage for the coupled system (Supplementary Fig. 4). The two curves intersected near 2.8 V and a power near 1.5 W, corresponding to a current density of about 0.5 A per 10 cm². At the intersection point, solar module and CO₂ electrolyser were optimally coupled and didn't require extensive regulation.

Reference electrodes, which would have allowed determination of the rate-limiting electrode, were not included in our devices, because we wanted to work at high current densities and, thus, with a very high gas load. At high current densities, conductivity of the electrolyte becomes one major contribution to energy losses, which can be roughly calculated from the distance between anode and cathode and the corresponding cell voltage (Figs. 2 and 3). CO₂ evolution (gas bubbles) on the anode side might be another loss channel (see Methods).

Conversion of syngas to acetate and ethanol. In a first experiment, syngas was produced by the PV-module-powered CO₂ electrolyser at a rate of 16.52 sccm and a composition of 11.76 % CO (4.8 mmol h⁻¹), 6.37 % H₂ (2.6 mmol h⁻¹) and 81.86 % CO₂ (33.4 mmol h⁻¹). This mixture was fed into two 1-litre fermenters, each with 0.5 litre culture at 36 °C, in which CO, H₂ and CO₂ were converted to acetate (reaction (1)) and ethanol (reaction (2)) by the activity of *C. autoethanogenum*^{11,29–32}. The acetogen can, like the closely related *C. ljungdahliae*, grow mixotrophically³³ and is amenable to genetic modification^{12,29}.



$$\Delta G^{\circ} = -94.6 \text{ kJ mol}^{-1}; \Delta H^{\circ} = -310.3 \text{ kJ mol}^{-1}$$



$$\Delta G^{\circ} = -29.7 \text{ kJ mol}^{-1}; \Delta H^{\circ} = -34.3 \text{ kJ mol}^{-1}$$

After 50 h of cell growth, stationary conditions were reached, where the cell concentration, the rates of CO and H₂ consumption

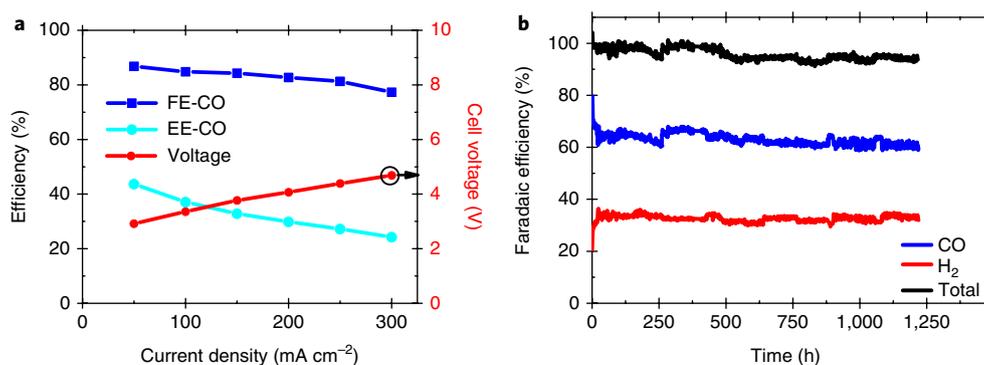


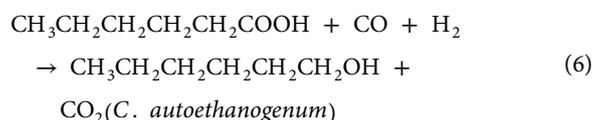
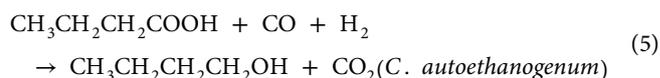
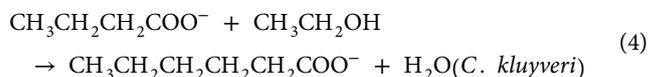
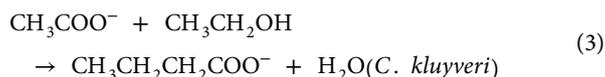
Fig. 3 | Further properties of the CO₂ electrolyser shown in Fig. 2a. **a**, Dependence of Faradaic efficiencies (FE) and energy conversion efficiencies (EE) on the electric current density (conditions as in Fig. 2a). The anolyte and the catholyte solutions, both 0.1 M K₂SO₄/1.5 M KHCO₃ (pH ≈ 7), were continuously cycled and mixed at a flow rate of 200 ml min⁻¹. The temperature was 30 °C. The gas diffusion electrode was operated at λ = 4.3, which corresponded to a CO₂ flow-rate of 90 sccm. **b**, Stability of the CO-FE and H₂-FE at an electric current density of 300 mA cm⁻². The cell voltage stayed constant within 7.0–7.5 V during the course of the experiment. The cathode and the anode were 9.5 mm apart and separated by a high-conductivity, zirconium-oxide-based diaphragm. The anolyte and the catholyte solutions, both 0.4 M K₂SO₄/0.5 M KHCO₃ (pH ≈ 7), were continuously cycled and mixed at a flow rate of 200 ml min⁻¹. The temperature was 30 °C. The gas diffusion electrode was operated at λ = 4.78, which corresponded to a CO₂ flow-rate of 100 sccm. H₂, CO and CO₂ concentrations were measured every 12 min.

and those of acetate and ethanol formation remained substantially constant for the next 45 h. The consumed CO and H₂ (3.35 mmol h⁻¹ in total) agreed well with the mol electron pairs (3.44 mmol h⁻¹) required to reduce CO₂ to acetate and ethanol (Table 2). The Faradaic efficiency (here the expression Faradaic efficiency is analogous to the characterization of the electrolyser) was almost 100%, indicating that essentially only acetate and ethanol were formed under the experimental conditions. The efficiency of energy conversion in syngas fermentation, calculated from the amount of ethanol produced (reactions (1) + (2)), was almost 80% (see Methods). Considering that the energy conversion efficiency of the CO₂ electrolyser at a low electric current density of about 50 mA cm⁻² was nearly 50% (Fig. 2c) and that of existing PV modules can be nearly 20%, the overall energy conversion efficiency of the described artificial photosynthesis system can be as high as 8% (Fig. 1). Similarly high conversion efficiencies have recently been described for a hybrid water splitting biosynthetic system involving *Ralstonia eutropha* for the reduction of CO₂ with H₂ to fuel alcohols^{34,35}, albeit at much lower electric current densities. An integrated electromicrobial conversion of CO₂ via formate to higher alcohols using recombinant *R. eutropha* strains also proceeded only at low current densities³⁶.

Besides acetate and ethanol, *C. autoethanogenum* is known to produce small amounts of 2,3-butanediol and lactic acid²⁹. These side products were, however, only formed in significant amounts when the CO concentration and the CO:H₂ ratio in the syngas were much higher.

Conversion of syngas to butanol and hexanol. In a second experiment, the CO₂ electrolyser was run at an electric current density of 150 mA cm⁻² (Supplementary Fig. 3b), resulting in a constant syngas production at a flow rate of 16.23 sccm and composition of 10% CO (4 mmol h⁻¹), 60% H₂ (24.2 mmol h⁻¹) and 30% CO₂ (12.2 mmol h⁻¹).

Again the syngas was fed into two 1-litre fermenters each with 0.5 litre *C. autoethanogenum* culture. 22 h later, the fermenters were additionally inoculated with *C. kluuyveri* cells. At the point of addition, the fermenter already contained acetate and ethanol, formed from CO, H₂ and CO₂ by the activity of *C. autoethanogenum* (reactions (1) and (2)). This inoculation led to the acetate and ethanol being converted to butyrate (reaction (3)) and hexanoate (reaction (4)) by *C. kluuyveri*^{37,38} and then to butanol (reaction (5)) and hexanol (reaction (6)) by *C. autoethanogenum*^{10,39–42}.



After steady state conditions were reached, the rates of CO and H₂ consumption and those of acetate and ethanol formation remained substantially constant for 45 h. The consumed CO and H₂

Table 2 | Acetate and ethanol formation by *C. autoethanogenum* from H₂, CO and CO₂ produced by the CO₂ electrolyser that was powered by electricity from a PV module

	H ₂	CO	ΣH ₂ +CO	C ₂ OOH	C ₂ OH	ΣC ₂
H ₂ and CO consumed and products formed (mmol h ⁻¹)	0.99	2.36	3.35	0.81	0.035	
Electron pairs recovered in products (mmol h ⁻¹)				3.24	0.21	3.44

50 h after inoculation of the fermenters with *C. autoethanogenum*, the cell concentration and the rates of gas consumption and of product formation were constant for at least 48 h thereafter. The rates within these 48 h were averaged. For details (time course, cell density, product distribution and substrate consumption rates) see Methods.

(14.88 mmol h⁻¹ in total) agreed well again with the mol electron pairs (14.52 mmol h⁻¹) required to reduce CO₂ to the three acids and alcohols (Table 3). The Faradaic efficiency was close to 100%. The energy conversion efficiency of formation of butanol and hexanol from CO, H₂ and CO₂ was nearly 78% (see Methods).

Interestingly, *C. carboxidovorans* alone can catalyse reactions (1)–(6)^{12,40}. However, the growth rate (0.023 h⁻¹) of this acetogen is far too low for a technical process.

Process design. As shown in Table 3, the conversion of CO, H₂ and CO₂ into butanol and hexanol can take place in a mixed culture of *C. autoethanogenum* and *C. kluyveri* under non-growth conditions. For an industrial process, however, it is important that the conversion takes place under chemostat (continuous) conditions and in two separate fermenters, as the optimum performance conditions of *C. autoethanogenum* and *C. kluyveri* differ. This is the basis for the design of an industrial process, forming butanol and hexanol at a scale of 10,000 tonnes per year (Supplementary Fig. 1). A prerequisite for a technical process is that the rate of carbon atoms being fixed in the gas fermenter is the same as the rate of carbon atoms being transformed to butanol and hexanol. For continuous fermentation, accumulation of the intermediates acetic acid and ethanol, as well as butyric acid and hexanoic acid, should be avoided. Here, we have shown experimentally that this prerequisite can be fulfilled (Supplementary Table 1).

To calculate the necessary current, pentanol is used as an example because it represents a 1:1 mixture of hexanol and butanol. Around 3.4×10^9 mol electrons are required to synthesize 10,000 tonnes pentanol. This means 328×10^{12} coulomb per year or 10.4×10^6 A (1 A = 1 C s⁻¹). At a minimal CO to H₂ consumption ratio of 1/5 in the fermentation (see reactions (9) and (10) in Methods), 16.7% of these electrons must be provided by the CO₂ electrolyser. It would possess a power of 8.2 MW ($4.7 \text{ V} \times 1.74 \times 10^6 \text{ A}$), assuming a supply voltage of 4.7 V (Fig. 2b). The remaining 83.3% of the required electrons are provided by the H₂O electrolyser, which at around 2.0 V, for example, would have to run at a power of 17.3 MW ($2.0 \text{ V} \times 8.66 \times 10^6 \text{ A}$). The overall plant would therefore consume $8.2 \text{ MW} + 17.3 \text{ MW} = 25.5 \text{ MW}$. This power could be provided by $14.6 \times 10^4 \text{ m}^2 = 14.6$ hectare PV modules with power density values of 175 W m^{-2} . Taking into account night-time, location and weather of the hypothetical plant, an area 5–10 times larger would be required (https://en.wikipedia.org/wiki/List_of_photovoltaic_power_stations).

For the example of the production of 10,000 tonnes of the alcohols, 568×10^6 mol (that is, 25,000 tonnes) of CO₂ are required. The CO₂ has to be fed into the CO₂ electrolyser at a rate of 1.1×10^3 mol min⁻¹, which is equal to a flow rate of 24.6×10^6 sccm (100% CO₂ at 10⁵ Pa). At 4.7 V (30 °C) and a λ of 4.3, the input CO₂ flow rate of our CO₂ electrolyser was 90 sccm (Supplementary Fig. 3). Therefore, the CO₂ electrolyser would have to be scaled up by a factor of 270,000. This can be achieved by increasing the electrode surface area from 10 cm² to 1 m² (factor 10³) and by stacking 270 electrolysis cells. Both of which in principle are possible and are being done.

In the fermenters, butanol and hexanol were produced together at a rate of 0.6×10^{-3} mol per hour per litre of culture (Supplementary Table 1). For the production of 10,000 tonnes of butanol and hexanol per year (that is, 12.9×10^3 mol alcohol per hour), the fermenters would have to be scaled up by a factor of 21.6×10^6 . This scale-up may be achieved by increasing the cell concentration in the fermenters by a factor of up to 30 and the volume from 1 litre to 700,000 litres, a volume not unusual in industrial fermentations^{43–47}. At this large volume it is advantageous that *C. autoethanogenum* and *C. kluyveri* grow in the fermenters in media containing only vitamins and minerals. The highly selective conditions make sterilization of the media unnecessary. This is especially important because it significantly reduces investment costs.

Another advantage of this set-up is that the products, butanol and hexanol, are easily extracted, allowing the unused media components to be easily recycled, which reduces the costs of water and media components. Butanol and hexanol are separated in two steps from the aqueous broth. The first step is to extract the alcohols using oleyl alcohol as an extracting solvent. The second step is to separate the alcohols from the solvent by distillation and recycle the solvent. The main energy consumption of this separation is the distillation step. To vaporize hexanol, 0.16 kWh kg^{-1} is needed, because of the vaporization enthalpy of 60 kJ mol^{-1} . In addition, the solvent has to be heated up to its vaporization temperature. This heat can only partly be recovered. Therefore, in sum roughly 0.6 kWh kg^{-1} hexanol energy is required to separate the products. This can be neglected compared to the energy consumed to synthesize the molecules, which is roughly 22 kWh kg^{-1} alcohol.

The advantages discussed above and the anticipated future low electricity costs (Fig. 1) all contribute to making this relatively small-scale approach competitive with traditional high-scale chemical productions of butanol and hexanol.

Under the experimental conditions described, butanol and hexanol were produced at almost the same rate (Supplementary Table 1). However, the ratio can be tuned, since it depends on the acetate to ethanol ratio⁴⁸, which in turn depends on the CO/H₂ ratio in the syngas²⁹. This is important since at present the butanol market¹ is larger than the hexanol market⁴⁹, but this may vary in future. Hexanol, apart from its present direct use in perfumes and other cosmetic applications, can be chemically dehydrated to 1-hexene⁵⁰ which is an important co-monomer for the production of polyethylene. Since hexanol is a liquid, it can also be easily transported to any polyethylene producer. Furthermore, hexanol could immediately substitute gasoline from fossil sources.

Other microorganisms can be combined with *C. autoethanogenum* instead of *C. kluyveri*, namely *Pelobacter propionicus*⁵¹, which ferments ethanol plus CO₂ to propionate and acetate or oleaginous yeast⁵², which convert ethanol and acetate to lipids. The right combination allows the production of various platform chemicals via artificial photosynthesis involving CO₂ electrolysis, as described here, at high Faradaic efficiencies.

Table 3 | Formation of acetate (C₂OOH), ethanol (C₂OH), butyrate (C₄OOH), butanol (C₄OH), hexanoate (C₆OOH) and hexanol (C₆OH) from H₂, CO and CO₂ by *C. autoethanogenum* plus *C. kluyveri*

	CO	ΣH ₂ +CO	C ₂ OOH	C ₂ OH	C ₄ OOH	C ₄ OH	C ₆ OOH	C ₆ OH	ΣC _{2,4,6}
H ₂ and CO consumed and products formed (mmol h ⁻¹)	2.08	14.88	1.45	0.6	0.21	0.14	0.05	0.04	
Electron pairs recovered in products (mmol h ⁻¹)			5.8	3.6	2.1	1.68	0.8	0.72	14.7

22 h after inoculation of the two fermenters with *C. autoethanogenum*, cells of *C. kluyveri* were added. 6 h later the rates of gas consumption and of product formation were found to be constant for at least 24 h (for details see text). The rates within these 24 h were averaged. For details (time course, cell density, product distribution and substrate consumption rates) see Methods.

Methods

The results reported above are examples. They are backed up, however, by many additional experiments performed under almost identical or very similar conditions leading to the same results.

Free energy and enthalpy changes are given under standard conditions: CO, H₂ and CO₂ as gas at 10⁵ Pa and acetate, ethanol, butyrate, hexanoate, butanol and hexanol at 1 molal solution.

The microfiltration system to retain the acetogenic cells in the gas fermenter (Supplementary Fig. 1) was developed for the improved fermentation of gaseous substrates⁵³.

Photovoltaic module. In our experiments the silicon PV modules were irradiated with a solar simulator with 1,000 W m⁻², simulating conditions on a sunny day with an air mass coefficient of 1.5 (standard test conditions). The temperature of the PV module was kept constant at 25 °C by a Peltier element. PV module (12.8 × 12.8 cm² = 164 cm²), from Conrad Electronics, consisted of 32 PV cells (1.7 × 2.6 cm²), each eight connected in series. At the maximum power point (1.8 W; Supplementary Fig. 4), the PV module delivered 482 mA per 10 cm² at 3.7 V and operated at a solar energy conversion efficiency of 11% (1.8 W × 100% / 16.4 W).

CO₂ electrolyser. Commonly, in CO₂ electrolysers the anolyte and catholyte contain mostly KHCO₃ at a pH around 7. The anolyte and catholyte are separated by a Nafion membrane. Due to the concentration difference of protons (10⁻⁷ M) and potassium cations (10⁻¹ M), the Nafion membrane is mostly potassium conducting. This leads to the following catholyte reaction: 3CO₂ + H₂O + 2e⁻ → CO + 2HCO₃⁻. With the potassium ions from the anolyte, the catholyte concentration of KHCO₃ increases proportional to the charge flow until precipitation. The anolyte reactions are as follows: H₂O - 2e⁻ → ½O₂ + 2H⁺ and 2HCO₃⁻ + 2H⁺ → 2CO₂ + 2H₂O. The concentration of KHCO₃ decreases proportional to the charge flow until all of the potassium cations have moved to the catholyte and only water is left as anolyte. To overcome this problem, two operation modes were tested: (i) in Supplementary Fig. 2a an almost continuous operation mode with sulfuric acid as the anolyte and KHCO₃ as the catholyte separated by a Nafion membrane is shown. Both anolyte and catholyte are running in separated cycles. However, with each proton, about four molecules of water are pulled through the membrane, which leads to a concentration of sulfuric acid in the anolyte and a dilution of KHCO₃ in the catholyte. (ii) The final solution is described schematically in Fig. 2a. In this set-up a mixture of KHCO₃ and K₂SO₄ is used both as catholyte and anolyte, which are mixed after each cycle with the result that cations, anions, pH and water remain balanced. A Nafion membrane is no longer needed and is replaced by a ZrO₂ diaphragm. Only the latter set-up is described here in more detail.

A commercial silver-based gas diffusion electrode (GDE) from Covestro, typically used as an oxygen depolarized cathode (ODC) in chloralkaline electrolysis^{24,54}, was used as cathode. The silver-based cathode is sensitive to H₂S (ref. 55) and other contaminants present in CO₂ obtained from cement and steel production, alcohol formation in breweries, anaerobic digestion plants and power plants converting biomass into electricity. Therefore, the CO₂ has to be freed of these contaminants before being used in the CO₂ electrolyser.

As anode, an Ir-MMO (iridium-mixed metal oxide) coated titanium sheet was used^{25,26}, which was purchased with the flow cell from ElectroCell. Such anodes are typically used in PEM type electrolysers (polymer / proton exchange membrane) for hydrogen production.

The aqueous catholyte and anolyte consisted of mixtures of KHCO₃ and K₂SO₄ (see captions of Figs. 2 and 3) at pH 7 without further additives. The conductivity was about 0.13 S cm⁻¹, which is low compared to alkaline hydrogen electrolysers (~1 S cm⁻¹). In CO₂ electrolysis, highly conductive catholytes like bases or acids cannot be used. While acids tend to form only H₂ at the cathode due to the high proton concentration, bases like KOH lead to the formation of CO₃²⁻ and HCO₃⁻. Neither can be reduced at the cathode and may form the salts K₂CO₃ or KHCO₃, which tend to crystallize and thus clog the GDE.

The electrolyte solutions were prepared with ultra-pure water (18.2 MOhm cm at 273 K, MilliQ Millipore system). Potassium hydrogen carbonate, potassium sulfate and sulfuric acid were used without further purification and were purchased from Alfa Aesar. All experiments were conducted by pre-saturating the electrolyte with CO₂ for 30 min.

All electrochemical experiments were conducted in a flow cell, which was purchased by ElectroCell (Micro Flow Cell) and slightly modified. This flow cell is a sandwich of three compartments with two liquid channels containing the catholyte and anolyte, and one CO₂ gas channel behind the cathode. The anode and the cathode compartments are separated by a ZrO₂ diaphragm. The surface area of each electrode was 10 cm². CO₂ gas (4.8 Linde) was used without further purification and continuously supplied at a constant flow rate controlled by a mass flow controller (Bronkhorst F-200CV-002-AAD-33-V) at atmospheric pressure. The flow rates are shown in the corresponding graphs.

A peristaltic pump (Ismatec ECOLINE VC-MS/CA8-6) was used to supply the electrolyte between the anode and GDE cathode at a flow rate of 200 ml per min. The flow rate had only minor effects on the CO Faradaic efficiency. The electrolyte reservoirs were magnetically stirred glass flasks held at a constant temperature

(30 °C) using a hot plate in combination with a glass-covered contact thermometer in the electrolyte. Contact between the electrolyte and any metal components was avoided to exclude contamination and a possible deactivation of the silver-based catalyst. These glass flasks were used for gas separation from the electrolyte. Contaminated GDEs form predominantly H₂.

The electrochemical flow reactor was operated using a potentiostat (Metrohm Autolab PGSTAT-30 with BOOSTER20A) under ambient pressure and temperature. Experiments were carried out in galvanostatic conditions, where a constant current is applied and the required voltage is monitored.

Conversion efficiency of the CO₂ electrolyser. The theoretical minimal cell voltage for the electrolysis of CO₂ to CO and O₂ is 1.34 V when calculated from $\Delta G^\circ = -258.5 \text{ kJ mol}^{-1}$ of the reaction: CO₂(g) → CO(g) + ½O₂(g) or from the redox potential difference $E_0' = +0.82 \text{ V}$ of the O₂/2H₂O couple and $E_0' = -0.52 \text{ V}$ of the CO₂/CO couple⁵⁶. Thus, at 3.65 V, the operation voltage of the CO₂ electrolyser when coupled to the PV module, electrolysis theoretically proceeds at an over potential of 2.3 V with an energy conversion efficiency of 37%. However, it is better to consider $\Delta H^\circ = -283.2 \text{ kJ mol}^{-1}$ of the reaction, which corresponds to an adiabatic minimal cell potential of 1.47 V. Otherwise an external heat source is needed to compensate an entropy increase. This limits the efficiency of the setup to 40% when 3.65 V is applied.

In the CO₂ electrolyser the distance between cathode and anode was 2 mm, which—depending on the electric current density—led to a significant ohmic loss. Ohmic losses were less at 60 °C than at 30 °C due to the higher conductivity of the electrolyte (Fig. 2b and Supplementary Fig. 2b).

Growth media. Medium A for *C. autoethanogenum* contained per litre composition: 1 g NH₄Cl, 0.1 g KCl, 0.2 g MgSO₄·7H₂O, 0.8 g NaCl, 0.1 g KH₂PO₄, 20 mg CaCl₂·2H₂O, 0.4 g L-cysteine-HCl, 0.4 g Na₂S·9H₂O, 20 mg nitrilotriacetic acid, 10 mg MnSO₄·H₂O, 8 mg (NH₄)₂Fe(SO₄)₂·6 H₂O, 2 mg CoCl₂·6 H₂O, 2 mg ZnSO₄·7H₂O, 0.2 mg CuCl₂·2H₂O, 0.2 mg Na₂MoO₄·2H₂O, 0.2 mg NiCl₂·6H₂O, 0.2 mg Na₂SeO₄, 0.2 mg Na₂WO₄·2H₂O, 20 µg biotin, 20 µg folic acid, 100 µg pyridoxine-HCl, 50 µg thiamine-HCl · H₂O, 50 µg riboflavin, 50 µg nicotinic acid, 50 µg Ca-pantothenic acid, 1 µg vitamin B₁₂, 50 µg p-aminobenzoic acid, 50 µg lipoic acid and 1 g yeast extract. The pH was adjusted to the pH indicated under continuous gassing.

Medium B for *C. autoethanogenum*, which differed from medium A mainly in not containing yeast extract, contained per litre composition: 0.5 g MgCl₂·6H₂O, 0.21 g NaCl, 0.135 g CaCl₂·2H₂O, 2.65 g NaH₂PO₄·2H₂O, 0.5 g KCl, 2.5 g NH₄Cl, 15 mg nitrilotriacetic acid, 30 mg MgSO₄·7H₂O, 5 mg MnSO₄·H₂O, 1 mg FeSO₄·7H₂O, 8 mg Fe(SO₄)₂(NH₄)₂·6H₂O, 2 mg CoCl₂·6H₂O, 2 mg ZnSO₄·7H₂O, 200 µg CuCl₂·2H₂O, 200 µg KAl(SO₄)₂·12H₂O, 3 mg H₃BO₃, 300 µg Na₂MoO₄·2H₂O, 200 µg Na₂SeO₄, 200 µg NiCl₂·6H₂O, 200 µg Na₂WO₄·6H₂O, 20 µg D-biotin, 20 µg folic acid, 10 µg pyridoxine-HCl, 50 µg thiamine-HCl, 50 µg riboflavin, 50 µg nicotinic acid, 50 µg Ca-pantothenate, 50 µg vitamin B₁₂, 50 µg p-aminobenzoate, 50 µg lipoic acid, 10 mg FeCl₃ with additional 500 mg L-cysteine-HCl. The pH was adjusted to 6 under continuous gassing.

Medium C for *C. kluyveri* contained per litre composition: 0.25 g NH₄Cl, 0.2 g MgSO₄·7H₂O, 0.31 g K₂HPO₄, 0.23 g KH₂PO₄, 2.5 g NaHCO₃, 1 g yeast extract, 10 g K-acetate, 20 g ethanol, 0.25 g L-cysteine-HCl, 1.5 mg FeCl₃·4H₂O, 70 µg ZnCl₂·7H₂O, 100 µg MnCl₂·4H₂O, 6 µg boric acid, 190 µg CoCl₂·6H₂O, 2 µg CuCl₂·6H₂O, 24 µg NiCl₂·6H₂O, 36 µg Na₂MoO₄·2H₂O, 3 µg Na₂SeO₄·5H₂O, 4 µg Na₂WO₄·2H₂O, 100 µg vitamin B₁₂, 80 µg p-amino-benzoic acid, 20 µg biotin, 200 µg nicotinic acid, 100 µg Ca-pantothenic acid, 300 µg pyridoxine-HCl, 200 µg thiamine-HCl · H₂O. The pH was adjusted to 7.5.

Conversion of syngas to acetate and ethanol. *C. autoethanogenum* (DSMZ 10061, Braunschweig) was routinely grown at 37 °C under continuous gassing with 67% H₂ and 33% CO₂ on medium A containing additionally 20 g l⁻¹ MES (adjusted to pH 6.0). The medium was then inoculated per litre with 100 ml of an active pre-culture grown to an OD₆₀₀ of 0.5 on the same medium. At an OD₆₀₀ of about 0.5, the cells were anaerobically harvested by centrifugation and the cell pellet from 100 ml culture re-suspended in 1 ml medium and the suspension then used to equally inoculate two 1 litre fermenters (run in series) each containing 500 ml of medium A and continuously gassed with syngas from the CO₂ electrolyser at a rate of 16.52 scfm and a composition of 11.76% CO (4.8 mmol h⁻¹), 6.37% H₂ (2.6 mmol h⁻¹) and 81.86% CO₂ (33.4 mmol h⁻¹).

In fermenter-1 the pH was kept constant at 5.5 and in fermenter-2 at 6.0 by the continuous addition of a base (anaerobic potassium hydroxide, 140 g l⁻¹) with a peristaltic pump. After 50 h of growth, the OD₆₀₀ in fermenter-1 increased from 0.05 to 1.3 and in fermenter-2 from 0.05 to 1.1 to then remain essentially constant for the next 45 h. In these 45 h, the flow rate of the gas coming out of the fermenters (16.03 scfm) and its composition of 6.03% CO (2.44 mmol h⁻¹), 3.96% H₂ (1.61 mmol h⁻¹) and 90.00% CO₂ (36.4 mmol h⁻¹) remained substantially constant, indicating a constant conversion rate of syngas into acetate and ethanol (Table 2).

Conversion of syngas to butanol and hexanol. The experimental setup was identical to that described for Table 2, except for the fact that the CO₂ electrolyser was powered at 5.4 V, resulting in an electric current density of 150 mA cm⁻².

At that time, cells of *C. kluyveri* (DSMZ 555, Braunschweig) were added and in medium A (see section 'Growth media') 20 g MES per litre was additionally present. The two 1-litre fermenters (run in series), each containing 500 ml medium, were gassed with 10% CO (4 mmol h⁻¹), 60% H₂ (24.2 mmol h⁻¹) and 30% CO₂ (12.2 mmol h⁻¹) from the CO₂ electrolyser at a flow rate of 16.23 sccm and then inoculated in equal parts with *C. autoethanogenum* cells harvested from 80 ml of an actively growing syngas culture (OD₆₀₀ = 0.62). After 22 h, the fermenters were additionally inoculated in equal parts with *C. kluyveri* cells harvested from 60 ml of a culture (OD₆₀₀ = 0.86) growing on ethanol and acetate. Six hours after the addition of the *C. kluyveri* cells, the rates of gas consumption and of product formation remained substantially constant for at least 24 h. In these 24 h, the flow rate of the outgoing gas (8.35 sccm) and its composition of 9.6% CO (2.0 mmol h⁻¹), 54% H₂ (11.3 mmol h⁻¹) and 36.4% CO₂ (7.6 mmol h⁻¹) remained substantially constant.

C. kluyveri was routinely grown on ethanol and acetate at 36 °C in medium C. The pH was adjusted to 7.5 and the medium then inoculated to an OD₆₀₀ of 0.1 with an actively growing pre-culture in the same medium. At OD₆₀₀ = 0.86, the cells from 60 ml of culture were anaerobically harvested by centrifugation and the cell pellet re-suspended in 10 ml of anoxic medium C and equal parts of the suspension used to inoculate the two fermenters.

Gas analysis. The product gases from the CO₂ electrolyser were measured with a Thermo Scientific Trace 1310 gas chromatograph (GC) equipped with two thermal conductivity detector (TCD) channels. The GC is directly connected to the experiment via a heated transfer line. For separation of CO₂, O₂, CO and hydrocarbons, a micropacked GC column (shin carbon) was used with He as carrier. The determination of H₂ was performed on a packed mol-sieve column using Ar as carrier. In the product gases from the cathode only CO and H₂ were detected by GC when using Ag as the catalyst. No traces of hydrocarbons (GC calibrated for CH₄, C₂H₄, C₂H₆, C₃H₄ down to 20 ppm) were detected. The cycle time of the GC was 12 min. The GC was calibrated biweekly. In relation to the fermenters, gas samples were taken before the first fermenter inlet and after the last fermenter gas outlet.

Solute analysis. Liquid samples were taken from the cultures via the sampling port of the fermenters and concentrations of acetate, butyrate, hexanoate, ethanol, butanol and hexanol were determined by quantitative ¹H NMR spectroscopy (Bruker AVANCE III HD, 600 MHz). Prior to quantitative analysis, samples were diluted with an adequate amount of phosphate buffer containing the internal standard trimethylsilyl propionate.

Calculation of energy conversion efficiencies. The energy conversion efficiency of the syngas fermentation to ethanol was calculated from the enthalpy changes (ΔH⁰) associated with reactions (1) and (2) and those associated with the combustion of H₂ (reaction (7)) and CO (reaction (8)).



$$\Delta G^0 = -474.3 \text{ kJ mol}^{-1}; \Delta H^0 = -571.7 \text{ kJ mol}^{-1}$$



$$\Delta G^0 = -514.4 \text{ kJ mol}^{-1}; \Delta H^0 = -565.9 \text{ kJ mol}^{-1}$$

Forming ethanol from 5H₂, CO and CO₂ (reaction (1) + (2)) is exothermic by -344.6 kJ mol⁻¹ to be compared with the enthalpy change of -1,711.2 kJ mol⁻¹ associated with the combustion of 5H₂ and 1CO (2.5 × reaction (7) + 0.5 × reaction (8)). Thus, when forming ethanol from syngas only (344.6/1,711.2) × 100 = 20.14% of the enthalpy change associated with the combustion of H₂ and CO is liberated as heat. Therefore, the efficiency of energy conversion in syngas fermentation to ethanol (reaction (1) + (2)) is almost 80%.

The energy conversion efficiency of the formation of butanol (reaction (9)) and hexanol (reaction (10)) from CO, H₂ and CO₂ was calculated from the enthalpy changes associated with reactions (7)–(10) to be near 78%. Reaction (9) = reactions (1), (2), (3) and (5); and reaction (10) = reactions (1), (2), (3), (4) and (6).



$$\Delta G^0 = -283.9 \text{ kJ mol}^{-1}; \Delta H^0 = -747.4 \text{ kJ mol}^{-1}$$



$$\Delta G^0 = -453.4 \text{ kJ mol}^{-1}; \Delta H^0 = -1152.4 \text{ kJ mol}^{-1}$$

Calculation of the alcohol yield per kWh. The amount of butanol and hexanol obtained per kWh by electroreduction of CO₂ was calculated as follows: butanol contains 24 mol electrons and hexanol 36 mol electrons per mol. Assuming butanol and hexanol are being formed at a molar ratio of 1:1 then per mol of the two alcohols 30 mol electrons are required from electricity. One mol of electrons equals 96,485.3 coulomb. One coulomb per second = 1 A. Per mol alcohols CO and H₂ are required in a molar ratio of 1:5. When the CO₂ electrolyser is run at

4.7 V (Fig. 2c) and the H₂O electrolyser at 2.0 V, then on average both together run at 2.45 V. One V·A = 1 W = 2.45 V·0.41 coulomb s⁻¹. In 1 h at 1 kW 0.41 coulomb add up to 1,475,000 coulomb = 15.29 mol electrons equivalent to 0.51 mol butanol/hexanol = 44.88 g butanol/hexanol.

Calculation of costs per kWh. The costs of butanol and hexanol obtained per kWh by electro-reduction of CO₂ was calculated from a price of 1 kWh = 2.5 cents (<http://cleantechies.com/2016/09/20/jinkosolar-marubeni-score-lowest-ever-solar-pv-at-us%C2%A22-42kwh-in-abu-dhabi>)⁵⁷ and from that of butanol = 1.2€ per kg (ref. ¹). The costs of CO₂ separation and purification are presently around 60€ per t = 0.276 cents per mol CO₂ (ref. ⁵⁸) but is expected to decrease significantly through improved separation and purification systems and carbon trading in the near future⁵⁹. For the synthesis of butanol and hexanol in a molar ratio of 1:1, 5 mol of CO₂ is required.

Data availability. All data are available from the corresponding author upon reasonable request.

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Author contributions

G.S. and R.W. discovered the potential of oxygen depolarized cathodes (ODC) for electrochemical CO₂-reduction. T.H. and M.D. are responsible for the fermentation part. G.S. and R.K. are responsible for the electrochemical part. M.D. and R.K. performed the laboratory work. G.S. and T.H. are heading the corresponding technology programmes at Siemens AG and Evonik Creavis GmbH, respectively, and wrote the paper.

Competing interests

The authors declare no competing financial interests.

Additional information

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Correspondence and requests for materials should be addressed to G.S.

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